

RYAZANTSEV, Sergey Nikolayevich; PAVLENKO, Viktor Fedorovich;

MALAYEVA, S.L., sostavitel' kart; DOBRONRAVOVA, K.O., red.;  
KONOVALYUK, I.K., mladshiy red.; KISELEVA, Z.A., red.kart;  
GLEBYKH, D.A., tekhn.red.

[Features of the economic geography of the Kirghiz S.S.R.]  
Kirgizskaia SSR; ekonomiko-geograficheskaiia kharakteristika.  
Moskva, Gos.izd-vo geogr.lit-ry, 1960. 483 p.

(MIRA 13:12)

(Kirghizistan--Economic geography)

RYAZANTSEV, Sergey Nikolayevich

Kirgizskaya SSR; ekonomiko-geograficheskaya kharakteristika, by S.N. Ryazantsev i V.F. Pavlenko. Moskva, Geografiz, 1960.

483 (I) p. illus., maps, tables.

At head of title: Akademiya Nauk SSSR. Institut Geografii.

Bibliography: p. 479-(484)

POPOV, A.; RYAZANTSEV, V.; KOMAROV, G.

Problems pertaining to the elevator storage of raw grain harvested  
in separate stages. Mik.-elev.prom. 25 no.3:19 Nr '59.  
(MIRA 12:6)

1. Dirketor Biyskogo elevatora (for Popov). 2. Biyskiy elevator,  
zamestitel' direktora po kachestvu (for Ryazantsev). 3. Zamestitel'  
nachal'nika Omskogo oblastnogo upravleniya khleboproduktov (for  
Komarov).

(Grain--Storage)

RYAZANTSEV, V. F. (Vet.)

"Treatment of parafilariaasis of horses."

SO: Vet. 26 (11) 1949, p. 45

RYAZANTSEV, V. F. (Vet.)

"The length of the viability of invasive larvae of strongylidae in soil."

SO: Vet. 29 (5), 1952, p. 45

Kuybyshev Veterinary Lab.

RYAZANTSEV, V.F., veterinarnyy vrach.

Weakening of the agglutination reaction in brucellosis of cattle  
on isolation farms. Veterinariia 30 no.8: 16-17 Ag '53.

(MLRA 6:8)

1. Veterinarnaya bakteriologicheskaya laboratoriya, Kuybyshev.

Ryzantsev, V. F.

80. Aerosol Control of Flies and Other Insects

"Aerosol Insecticidal Pots for the Control of Flies," by V. F. Ryazantsev, a Veterinary Physician, Veterinariya, Vol 34, No 6, Jun 57, pp 61

Reports the use of insecticidal hexachlorane pots NBK-G-17 for the control of flies, mosquitos, gnats, gadflies, and other insects. These pots contain a thermic mixture which on burning develops a high temperature. The heat vaporizes the hexachlorane, which becomes condensed in air forming highly dispersed aerosols in the form of an insecticidal smoke.

V. A. Nabokov, I. I. Gadanina, and others found the insecticidal smokes to be effective in the control of Ixodidae ticks. V. I. Kurchatov and V. I. Vashkov established that hexachlorane in aerosol state and in concentrations now used is not toxic to warm blooded animals. Experiments conducted in 1956 determined that the Hexachlorane Pots NBK G-17 were effective as fumigants of livestock shelters. Persons working with aerosol insecticide pots must observe all safety and fire regulations. (U)

Sum 1424

*RYAZANTSEV, V.F.*  
RYAZANTSEV, V.F., podpolkovnik meditsinskoy sluzhby; ORLOV, P.M.; ALAD'YEV, N.G.

Aerosol insecticide pots in fly control. Voen.-med.zhur. no.7:85  
Jl '57. (MIRA 11:1)

(AEROSOLS) (INSECTICIDES) (FLIES)

RYAZANTSEV, Ye.A., inzh.

Introduction of remote control and results of operating remote  
control devices in Municipal Electric Power Systems. Trudy VNIIE  
no.7:27-33 '58. (MIRA 16:12)

RYAZANTSEV, V.I.

Sea maps with radiolocational elements of the area. Geog.shor.  
no.13:135-149 '59. (MIRA 12:6)  
(Nautical charts) (Radar in navigation)

RYAZANTSEV, V. I., kand. voyenno-morskikh nauk

Representing the underwater relief by isobaths. Geod. 1 kart  
no. 49-57 Ap '60. (MIRA 13:8)  
(Hydrographic charts)

RYAZANTSEV, V. I., MORACHEVSKIY, I. I., and SPEKTER, B. E.

"Method and Instrument for the Determination of Thermal Properties of Materials without Testing."

Report submitted for the Conference on Heat and Mass Transfer, Minsk, BSSR, June 1961.

MORACHEVSKIY, I. I.; SPEKTOR, B. V.; RYAZANTSEV, V. I.

A method and instrument for determining the thermophysical characteristics of materials without taking samples. Teplo-  
i massoper. 1:61-64 '62. (MIRA 16:1)

1. Nauchno-issledovatel'skiy institut stroitel'nykh materialov  
Akademii stroitel'stva i arkhitektury UkrSSR.

(Materials--Thermal properties)  
(Materials--Testing)

DUGANOV, G.V., doktor tekhn.nauk; SPEKTOR, B.V., kand.khim.nauk;  
RYAZANTSEV, V.I., inzh.; NIKITIN, A.I., inzh.

Using the TP-1 device for rapid determining of the thermal characteristics of coals and rocks. Ugol'.prom. no.4:69-70 (MIRA 15:8)  
Jl-Ag '62.

1. Dnepropetrovskiy gornyy institut im. Artema i Nauchno-issledovatel'skiy institut stroitel'nykh materialov Akademii stroitel'stva i arkhitektury UkrSSR.  
(Rocks--Thermal properties) (Electronic instruments)

DUGANOV, G.V.; NIKITIN, A.N.; RYAZANTSEV, V.I.; SPEKTOR, B.V.

Rapid determination of thermophysical properties of rocks in a  
massif. Izv. vys. ucheb. zav.; tsvet. met. 5 no.4:14-20 '62.

(MIRA 16:5)

1. Dnepropetrovskiy gornyy institut, kafedra rudnichnoy ventilyatsii.  
(Rocks—Thermal properties)

SPEKTOR, B.V.; RYAZANTSEV, V.I.; KOZACHENKO, G.A.

Automatic instrument for determining the coefficient of heat conductivity of building materials and heat insulating materials. Zav.lab. 28 no.1:104-105 '62. (MIRA 15:2)

1. Nauchno-issledovatel'skiy institut stroitel'nykh materialov i izdeliy Akademii stroitel'stva i arkhitektury USSR.  
(Building materials--Thermal properties)  
(Insulating materials--Testing)

S/032/63/029/004/006/016  
A004/A127AUTHORS: Spektor, B.V., Ryazantsev, V.I., Kozachenko, G.A.

TITLE: Automation of the process of determining the coefficient of temperature conductivity of materials

PERIODICAL: Zavodskaya laboratoriya, no. 4, 1963, 447 - 449

TEXT: The coefficient of temperature conductivity is calculated by the equation  $a = K \cdot \frac{\ln t_1 - \ln t_2}{\tau_2 - \tau_1}$ , where K = coefficient of the body shape, which is determined by shape and dimensions of the specimen;  $t_1$  and  $t_2$  = temperature difference between specimen center and surrounding medium at  $\tau_1$  and  $\tau_2$  respectively. If the temperature measurements at the given time  $\tau_1$  and  $\tau_2$  can be automated and magnitude  $t_1$  maintained constant, it is possible to fully automate the process of determining the coefficient of temperature conductivity by the method of regular heat-exchange conditions. The authors suggest the design of an automatic installation for these measurements based on the ЭПБ-01 (EPV-01) electronic potentiometer, in the housing of which

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Automation of the process of ...

S/032/63/029/004/006/016  
A004/A127

two time relays, an PHT-100 (RPT-100) electromagnetic relay, a contact group and an electromagnet are installed. The electric block diagram is presented and the operation of the device described. Tests showed that the straggling of results does not exceed  $\pm 1.6\%$ . There is 1 figure.

ASSOCIATION: Nauchno-issledovatel'skiy institut stroitel'nykh materialov i izdeliy Akademii stroitel'stva i arkhitektury UkrSSR  
(Scientific-Research Institute of Structural Materials and Components of the Academy of Construction and Architecture UkrSSR)

Card 2/2

PROCESSES AND PROPERTIES INDEX

10

ca

Synthesis of methyl vinyl ketone by hydration of vinylacetylene under pressure. A. N. Churibakov and V. N. Ryzantsev. *Org. Chem. Ind. (U. S. S. R.)* 7, 0933-6 (1940); *cf. C.A.* 35, 3961P. — (1) *Hydration at room temp.*—Vinylacetylene and a H<sub>2</sub>SO<sub>4</sub> soln. of HgO were cooled to -10° and charged into a bakelite-lined Fe tube 200 mm. high and 40 mm. in diam. and shaken for 3 hrs. while hermetically sealed. The max. temp. did not exceed 40°. A max. yield of Me vinyl ketone of 65.8% was obtained under the following conditions: HgO 5.5, H<sub>2</sub>SO<sub>4</sub> (d. 1.84) 0.4, vinylacetylene 26 and water 100 g. In the absence of HgO the vinylacetylene was not hydrated. (2) *Hydration at high temps.*—Reaction was carried out in a bakelite-lined autoclave which was heated by a water bath. The previously cooled compds. were charged into the autoclave, the temp. was raised to the desired point and the stirrer started. The temp. of the water bath varied from 42° to 68°. A max. yield of 77.2% Me vinyl ketone on the basis of the vinylacetylene was obtained under the following conditions: HgO 17 g., temp. of bath 55-58°, duration of reaction 105 min. The yield of Me vinyl ketone on HgO was greatest (19.1 g./g.) under these conditions: HgO 10 g., temp. of bath 48-48°, duration of reaction 34.5 min. On the basis of vinylacetylene the yield was 07.9%. On the basis of the HgO used the process is best carried out with HgO 10, H<sub>2</sub>SO<sub>4</sub> (d. 1.84) 270, water 1000 and vinylacetylene 259 g., temp. of bath 50-58°, duration of reaction 333 min. The yield of ketone was 24.0 g./g. of HgO. B. Z. Kamich

METALLURGICAL LITERATURE CLASSIFICATION

ASB. 35.A

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

1ST AND 2ND ORDERS

PROCESSES AND PROPERTIES INDEX

10

CA

The synthesis of methyl vinyl ketone by hydration of vinylacetylene. A. N. Churbakov and V. N. Ryazantsev. *J. Applied Chem. (U. S. S. R.)* 13, 1464-9 (in French, 1460) (1940).—The hydration of vinylacetylene was carried out by the Kucherov method (C. A. 3, 2682). The optimal conditions were: compn. of the hydration mixt. 1 g. HgSO<sub>4</sub>, 3.4 g. H<sub>2</sub>SO<sub>4</sub> (d. 1.84) and 51 g. water, and initial temp. of the reaction 60-62°, yielding 80% of Me vinyl ketone (by wt. of reacted vinylacetylene). The yield was increased to 83% by introducing Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub>. The yield decreased in the ratio HgSO<sub>4</sub>:Fe<sub>2</sub>(SO<sub>4</sub>)<sub>3</sub> = 1:3. The yield decreased during carrying out the reaction without an excess of vinylacetylene. Butanone was identified in the by-products of the reactions. Hg formed by the reduction of HgSO<sub>4</sub> during the reaction can be recovered to the extent of 94% from the residue of the reaction. A. A. Podgorny.

358.514 METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS

L 39777-66 ENT(m)/ETD(f)  
ACC NR: AT6012692

CD-2

SOURCE CODE: UR/3136/65/000/991/0001/0044

AUTHOR: Goncharov, V. V.; Babulevich, Ye. N.; Shavrov, P. I.; Ryazantsev, Ye. P.  
Novikov, I. M.; Yegorenkov, P. M.; Chervyatsov, A. A.; Frolov, I. P.; Zhigachev,  
V. M.; Pushnin, B. T.; Fischevskiy, V. K.; Zakharov, L. K.; Kruglov, A. B.; Karasev,  
N. A.; Goncharov, L. A.

ORG: State Committee on the Use of Atomic Energy SSSR, Institute of Atomic Energy  
im. I. V. Kurchatov, Moscow (Gosudarstvennyy komitet po ispol'zovaniyu atomnoy  
energii SSSR, Institut atomnoy energii)

TITLE: Experience in operation of the MR reactor and tests of fuel elements and materials

SOURCE: Moscow. Institut atomnoy energii. Doklady, no. 991, 1965. Opyt eks-  
pluatatsii reaktora MR i provedeniye ispytaniy TVEL i materialov, 1-44

TOPIC TAGS: nuclear research reactor, reactor fuel element, nuclear reactor  
material, nuclear reactor characteristic

ABSTRACT: The authors discuss the loop research reactor MR constructed at the  
Kurchatov Institute of Atomic Energy and intended for the test of fuel elements  
and materials in new atomic installations. It is described in paper P/323 of the  
Third Geneva Conference in 1964. The present article describes in detail its con-

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22  
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L 39777-65  
ACC NR: AT6012692

struction and the various test loops in it. The section headings are: I - Introduction. II. Operation of reactor. 1. Certain physical characteristics of the reactor. a) Fuel burnup. b) Efficiency of control valves, scram rods, and movable fuel assemblies. c) Fluxes of thermal and fast neutrons. 2. Control and protection system of the reactor. 3. Technological systems of the reactor. a) Cooling loop for fuel element assembly. b) Cooling loop for the reactor assembly blocks. c) Intermediate (second) cooling loop of reactor. d) Third cooling loop of reactor. e) Water purification system. 4. Fuel assembly operating conditions and conditions for the graphite stacking blocks. 5. Reloading operations. III. Operation of loop installations. Organization and performance of tests on fuel elements and materials. IV. Dosimetric control. Radiation shielding of reactor. The reactor has been in operation since 24 July 1964, and its power has been gradually increased from the initial 20 MW to 30 MW. The usual operation is at 25 MW. The reactor has 3 loop channels with 7 associated experimental channels. Various characteristics of the reactor at different power ratings are tabulated. Major contributions to the adjustment of the MR reactor were made by A. Ye. Alekseyev, B. A. Alekseyev, S. N. Begichev, A. B. Bugayenko, Yu. I. Kovalev, V. K. Lebedev, A. M. Rotankov, V. D. Rusov, N. V. Sarychev, Ye. S. Chernorotov, and Yu. A. Shikov.

Orig. art. has: 13 figures and 6 tables.

SUB CODE:           SUBM DATE: 00/   ORIG REF: .001

Card 2/2772

L 37689-65 EPA/EPF(c)/EPR/EPA(e)-2/EWT(m)/EWA(o) Pr-4/Pt-10/Paa-4 WW/JDW

ACCESSION NR: AP5009543

S/0207/65/000/001/0057/0061

AUTHOR: Novikov, S. S. (Moscow); Ryazantsev, Ye. S. (Moscow)

45  
B

TITLE: Theory of combustion stability of solid propellants

SOURCE: Prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 1, 1965, 57-61

TOPIC TAGS: combustion stability theory, solid propellant, combustion stability criterion, combustion stability, combustion

ABSTRACT: Mathematical criteria of the combustion stability of solid propellants were derived for the zero- and 1st-order reactions in Q-model combustion (when the gasification of the condensed phase (k-phase) occurs as a result of the exothermic reaction in the k-phase) and for the zero- and 1st-order reactions in T<sub>g</sub>-model combustion (when the gasification of the k-phase occurs as a result of the surface, gaseous-phase temperature, T<sub>g</sub>). The proposed combustion stability theory takes into account the heat generated in the k-phase. The effect of the heat generated in the surface layer of the k-phase and the temperature fluctuations in the gaseous phase near the charge surface on the combustion stability of solid propellants is discussed. [PS]  
Orig. art. has: 1 figure and 21 formulas.

Card 1/2

MAMCHENKO, V.P., inzh.; RYAZANTSEVA, T.A., inzh.; DROZDOV, B.A., kand. tekhn. nauk, retsenzent; RYZINBOD, S.Ya., kand. tekhn. nauk, retsenzent; POLULEKH, V.K., inzh., retsenzent; STOLYARCHUK, I.V., kand. tekhn. nauk; GOROKHOVIKOV, L.M., kand. tekhn. nauk; SAZONOV, A.G., inzh., red.; CHEREPASHENETS, R.G., inzh., red.; USENKO, L.A., tekhn. red.

[Operation of locomotives] Ekspluatatsiia lokomotivov. Moskva, Transzheldorizdat, 1963. 415 p. (MIRA 16:12)  
(Locomotives) (Railroads--~~Man~~)

AMERIK, B.K.; GALEYEVA, K.S.; USPENSKIY, G.I.; RYAZANTSEV, Yu.P.;  
MUSNIKOVA, D.M.; ANTOSHKINA, R.A.

Contact coking of a cracking residue in a mixture with  
powdered coke on a pilot plant. Trudy GrozNII no. 15:68-  
74 '63. (MIRA 17:5)

RYAZANTSEV, Yu.P.; VAYNSHTEYN, TS.V.

Investigating the kinetic laws of the burning of granulated  
petroleum coke. Trudy GrozNII no. 15:111-118 '63.

(MIRA 17:5)

AMERIK, B.K.; RYAZANTSEV, Yu.P.; DROZDOVA, Ye.I.; KHALOIMENKO, N.N.

Designing apparatus for contact pyrolysis. Trudy GrozNII  
no. 15:75-82 '63. (MIRA 17:5)

L 33377-66 EWP(m)/EWT(1)/EWT(m)/T WPI/JWD  
ACC NR: AP6021362 SOURCE CODE: UR/0207/66/000/003/0137/0139

AUTHOR: Novikov, S. S. (Moscow); Ryazantsev, Yu. S. (Moscow)

43  
K

ORG: none

TITLE: Remarks concerning gun powder combustion stability theory

SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 3, 1966, 137-139

TOPIC TAGS: gun powder, combustion stability, combustion theory

ABSTRACT: The results of previous theoretical studies of the combustion stability of gun powders (Istratov A. G., Librovich V. B. PMTF, 1964, no. 5; Novikov S. S., Ryazantsev Yu. S., PMTF, 1965, no. 1; Novozhilov B. V., PMTF, 1965, no. 4) are verified by using the Laplace transformation method. The authors thank A. G. Istratov, V. B. Librovich, and A. I. Leonov for their comments. Orig. art. has: 12 formulas. [PS]

SUB CODE: 19/ SUBM DATE: 10Feb66/ ORIG REF: 008/ ATD PRESS: 5026

Card 1/1 JS

L 26254-66 EWP(m)/EPF(n)-2/EWA(h)/EWT(1)/EWT(m)/ETC(m)-6/T/EWA(d)/EWA(1) IJP(c)

ACC NR: AP6013924 WW/JW/JWD/WE SOURCE CODE: UR/0207/66/000/002/0057/0062

AUTHOR: Novikov, S. S. (Moscow); Ryazantsev, Yu. S. (Moscow)

ORG: none

TITLE: Interaction of sound waves with burning surface of condensed systems

SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 2, 1966, 57-62

TOPIC TAGS: condensed explosive, combustion instability, sound wave, acoustic admittance, solid propellant

ABSTRACT: The problem of the acoustic admittance of burning surfaces of condensed explosives and the effect of reflected sound waves on the combustion stability were studied theoretically. The exothermic reaction in the condensed phase, its effect on the burning velocity, and the change in the condensed phase surface temperature under nonsteady-state conditions were taken into account. A theoretical model of the combustion process was used in which the burning zone consisted of 5 regions: 1) a heating region in the condensed phase without a chemical reaction 2) a chemical reaction region in the condensed phase; 3) a heating region of the gas phase also without a chemical reaction; 4) a chemical reaction region in the gas phase; and 5) a region with gaseous combustion products. Equations describing the linear perturbation of the combustion parameters in regions 1-4 at a harmonic pressure change were derived. Acoustic properties of the burning surface of the

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ACC NR: AP6013924

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condensed phase are characterized by the acoustic admittance of the burning surface, for which an equation was also derived. The combustion instability of condensed explosives is connected with the amplification of sound waves reflected from the burning surface. The conditions under which sound wave amplification takes place are given. Values of several dimensionless parameters were calculated and plotted. A comparison of the calculated data with corresponding published experimental data for ballistic powders showed good agreement for high-pressure combustion. There is a marked disagreement between the experimental and theoretical data obtained for low-pressures. Orig. art. has: 2 figures, 2 tables, and 14 formulas. [PS]

SUB CODE: 21, 19/ SUBM DATE: 21Dec65/ ORIG REF: 011/ OTH REF: 003/ ATD PRESS

4243

Card 2/2 CC

RYAZANKIN, Vladimir Nikolayevich; YEVSTIGNEYEV, German Pavlovich;  
TRESBYATSKIY, Nikolay Nikolayevich [deceased]; DOBROGURSKIY,  
S.O., professor, doktor tekhnicheskikh nauk, redaktor; DOSTUPOV,  
B.G., kandidat tekhnicheskikh nauk, retsenzent; DOBROSMYSLOV, V.I.  
inzhener, retsenzent; POLYAKOV, G.F., redaktor izdatel'stva;  
SOKOLOVA, T.F., tekhnicheskiy redaktor

[Calculating machines] Vychislitel'nye mashiny. Pod red. S.O.  
Dobrogurskogo. Moskva, Gos. nauchno-tekhn. izd-vo mashinostroit.  
lit-ry, Pt. 1. [Calculating machines with keys] Vychislitel'nye  
klavishnye mashiny. 1957. 251 p. (MLRA 10:5)  
(Calculating machines)

RYAZANOV, Vladimir Aleksandrovich

8.3-26

551.510.42(02)

Ryazanov, Vladimir Aleksandrovich. *Sanitarnaya okhrana atmosfernogo vozdukh.* [Sanitary protection of the air.] Moscow, Gosud. Izdat, 1954. 235 p. 20 figs., 52 tables, bibliog. p. 227-231. **DLC**—A well compiled manual on the sanitary protection of atmospheric air giving a detailed picture of the present state of the problem in the Soviet Union and discussing, on the basis of latest advances, the permissible limits of air pollution and the measures to be taken in order to combat air pollution in cities and industrial centers by the State Sanitary Inspection. Pt. I of the book (2 chapters) deals with general problems of atmospheric hygiene, laws of smoke propagation in the air, and principles of hygienic standardization of atmospheric pollution. Pt. II, Air pollution by dust and its prevention includes: Ch. 3, Atmospheric dust and its properties; Ch. 4, Methods of determining the degree of air pollution by dust; Ch. 5, Fuel combustion as the main source of air pollution; Ch. 6, Other (industry) sources of air pollution; Ch. 7, Preventive measures against dust pollution. Pt. III, Air pollution by gases and vapors and its prevention, contains: Ch. 8, Air pollution with sulfur dioxide and other sulfur compounds; Ch. 10, Air pollution by other chemical substances, hydrogen chloride, carbon monoxide, and many others). The book concludes with some remarks on the State Sanitary Inspection of the air. Review by M. S. Gol'dberg in *Gigiena i Sanitariia*, Moscow, 21(9):59-60, Sept. 1956. **Subject Headings:** 1. Atmospheric pollution control 2. U.S.S.R.—A.M.P.

RYAZANTSEV, B.S.

ALFEROV, A.A.; ARTEMKIN, A.A.; ASHKENAZI, Ye.A.; VINOGRADOV, G.P.; GALEYEV, A.U.; GRIGOR'YEV, A.N.; D'YACHENKO, P.Ye.; ZALIT, N.N.; ZAKHAROV, P.M.; ZOBNIN, N.P.; IVANOV, I.I.; IL'IN, I.P.; KMETIK, P.I.; KUDRYASHOV, A.T.; LAPSHIN, F.A.; MOLYARCHUK, V.S.; PERTSOVSKIY, L.M.; POGODIN, A.M.; RUDOY, M.L.; SAVIN, K.D.; SIMONOV, K.S.; SITKOVSKIY, I.P.; SITNIK, M.D.; TETREEV, B.K.; TSETYRAIN, I.Ye.; TSUKANOV, P.P.; SHADIKYAN, V.S.; ADELUNG, N.N., retsenzent; AFANAS'YEV, Ye.V., retsenzent; VLASOV, V.I., retsenzent; VOROB'YEV, I.Ye., retsenzent; VORONOV, N.M., retsenzent; GRITCHENKO, V.A., retsenzent; ZHEREBIN, M.N., retsenzent; IVLIYEV, I.V., retsenzent; KAPORTSEV, N.V., retsenzent; KOCHUROV, P.M., retsenzent; KRIVORUCHKO, N.Z., retsenzent; KUCHKO, A.P., retsenzent; LOBANOV, V.V., retsenzent; MOROZOV, A.S., retsenzent; ORLOV, S.P., retsenzent; PAVLUSHKOV, E.D., retsenzent; POPOV, A.N., retsenzent; PROKOF'YEV, P.F., retsenzent; RAKOV, V.A., retsenzent; SINEGUBOV, N.I., retsenzent; TERNIN, D.F., retsenzent; TIKHO-MIROV, I.G., retsenzent; URBAN, I.V., retsenzent; FIALKOVSKIY, I.A., retsenzent; CHEPYZHEV, B.F., retsenzent; SHEBYAKIN, O.S., retsenzent; SHCHERBAKOV, P.D., retsenzent; GARNYK, V.A., redaktor; LOMAGIN, N.A., redaktor; MORDVINKIN, N.A., redaktor; NAUMOV, A.N., redaktor; POBEDIN, V.F., redaktor; RYAZANTSEV, B.S., redaktor; TVERSKOY, K.N., redaktor; CHEREVATYY, N.S., redaktor; ARSHINOV, I.M., redaktor; BABELYAN, V.B., redaktor; BERNGARD, K.A., redaktor; VERSHINSKIY, S.V., redaktor; GAMBURG, Ye.Yu., redaktor; DERIBAS, A.T., redaktor; DOMBROVSKIY, K.I., redaktor; KORNEYEV, A.I., redaktor; MIKHEYEV, A.P., redaktor

(Continued on next card)

ALFEROV, A.A. ---- (continued) Card 2.

MOSEKVIN, G.N., redaktor; RUBINSHTEYN, S.A., redaktor; TSYPIN, G.S.,  
redaktor; CHERNYAVSKIY, V.Ya., redaktor; CHERNYSHEV, V.I., redaktor;  
CHERNYSHEV, M.A., redaktor; SHADUR, L.A., redaktor; SHISHKIN, K.A.,  
redaktor

[Railroad handbook] Spravochnaia knizhka zheleznodorozhnika. Izd.  
3-e, ispr. i dop. Pod obshchei red. V.A.Garnyka. Moskva, Gos.  
transp.zhel-dor. izd-vo, 1956. 1103 p. (MLRA 9:10)

1. Nauchno-tekhnicheskoye obshchestvo zheleznodorozhnogo transporta.  
(Railroads)

RYAZANTSEV, V.V.

Work of Diesel Assembly on the conversion of diesels to gas.  
Biul.Kom.po gazosil.ust. no.2:37-39 '47. (MLRA 9:12)

1.Dizel'montazh Narodnogo Komissariata tyazhelogo mashino-  
stroyeniya SSSR.  
(Diesel engines)

PA 161T57

USSR/Engineering - Engines, Clark-Bross  
Metallurgy May 50

"Replacing Cylinders of Clark-Bross Engines," V. V. Ryzantsev, 7 1/2 pp

"Energet Byul" No 5

Criticizes Clark-Bross RAD and D-9 engines for: unit-casting of lower part of cylinder, bushing and jacket; appearance of cracks in jacket, bushing partly to local thinness of cylinder walls. D-9 cylinders (modified by Dizelmontazh, D-9-4, 1948) with removable bushings have run successfully over 1,000 hr; modified RAD ready for tests. Suggests

FDD

161T57

USSR/Engineering - Engines, Clark-Bross May 50  
(Cont'd)

Remodeling Clark engines. Gives calculations for speed of water flow, data for pressures, stresses, etc. Cylinder jackets must be made of Sch 21-40 steel; studs, of 40KhM alloy steel (GOST 45-4328) or high-grade carbon steel with increased manganese content (e.g., 35G2); bushings, of Sch 24-44 steel.

FDD

161T57

6(6)

05204  
SOV/142-2-3-12/27

**AUTHORS:**

Budov, A.F., Butrim, Yu.I., Kovtun, P.S., Ryazantsev, V.Yu.,  
Yanovskiy, V.

**TITLE:**

Experimental Industrial Television Devices

**PERIODICAL:**

Izvestiya vysshikh uchebnykh zavedeniy, Radiotekhnika, 1959, Vol  
2, Nr 3, pp 361-363 (USSR)

**ABSTRACT:**

The authors describe briefly the experimental industrial television equipment "Ekran-1", "Ekran-2" and "Ekran-3" which were developed at the Kafedra radiotekhnicheskikh ustroystv Khar'kovskogo polytechnicheskogo instituta imeni V.I. Lenina (Chair of Radio Engineering Equipment of the Khar'kov Polytechnic Institute imeni V.I. Lenin). The device "Ekran-1" was developed in 1956 for the visual control of the work of cutting tools on heavy boring and turning mills with two tool rests. The cameras have the dimensions 170x159x355 mm and a weight of 7 kg. They are mounted directly at the tool rests. The camera commutator unit, the control panel with the TV screen are mounted at the master control panel of the machine tool. During 1957 and 1958 the experimental industrial TV devices "Ekran-2" and "Ekran-3" were developed. These devices are

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SOV/142-2-3-12/27

Experimental Industrial Television Devices

more universal and produce high-quality images at a distance of 100-150 m. Additional conventional TV sets may be used at distances of up to 1 km from the control unit. The "Ekran-2" may be used for televising surgical operations. Fig.1 shows the TV camera used for the "Ekran-2" and "Ekran-3". It has the dimensions 110 x 120 x 300 mm and a weight of 3.5 kg. A vidicon pick-up tube is used. A 500 watt light source provides the necessary illumination of 500-1000 lux. With such an illumination the inertia of the vidicon tube is very low and even high-speed production processes may be observed clearly. All TV devices have interlaced image scanning of 600-626 lines. The receiver units of "Ekran-2" and "Ekran-3" are shown by photographs in figs.2 and 3. The interlacing parameters correspond to the USSR TV standard. The synchrogenerator of the industrial TV devices produces a simplified TV signal required for the synchronization of the additional TV sets connected to these devices. The synchrogenerator is composed of ten 6N1P tubes (including cathode followers). The number of bulky parts in the camera units was reduced to a minimum. The focussing of the pick-up tube is achieved by an electric motor operated from the control

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SOV/142-2-3-12/27

Experimental Industrial Television Devices

panel. The conventional TV sets which may be connected to the "Ekran-2" and "Ekran-3" are fed from a transmitter, consisting of a master oscillator-multiplier (6Zh3P) and an output stage (6Zh2P). The "Ekran-2" device contains provisions for transmitting audio frequencies to the conventional TV sets connected to it. All TV devices receive power from the AC mains. In the "Ekran-1" and "Ekran-2" the feed units contain heater transformers and kenotron rectifiers with electronic stabilization which feed all anode circuits. In the "Ekran-3" germanium and selenium rectifiers are used. Electronic stabilization is used only for feeding the synchronization unit and the camera amplifier. A ferro-resonance voltage stabilizer feeds the entire device. All "Ekran" devices contain only four or five control knobs. The publication of this article was recommended by the Kafedra radiotekhnicheskikh ustroystv Khar'kovskogo instituta imeni V.I. Lenina (Chair of Radio Engineering of the Khar'kov Polytechnic Institute imeni V.I. Lenin). There are 4 photographs.

Card 3/3

SUBMITTED: July 24, 1958

RYAZANTSEV, Ya.

Instrument for testing the air-tightness of storage batteries.  
Avt.transp.32 no.12:31 D '54. (MIRA 8:3)  
(Automobiles--Batteries)

RYAZANTSEV, Ye.

Install a voltammeter on cars. Avt.transp. 32 no.7:35 J1 '54.  
(MIRA 7:9)

(Automobiles--Electric equipment) (Voltmeter) (Ammeter)

PA 1/50197

RYAZANTSEV, Yu.

USSR/Radio - Radio, Training  
Radio Receivers

Sep 49

"Training New Radio Experts," Yu. Ryzantsev,  
Champion of Saratov Oblast in Short-Wave Re-  
ception, Mem. Con and Saratov Radio Clubs of  
DOBARM, 1 p

"Radio" No 9

In connection with the patriotic movement to  
train a new corps of Soviet radio technicians,  
author has pledged to: (1) train five young  
radio amateurs of the city of Engel for par-  
ticipation in the Ninth All-Union Corr Radio  
Exhibit, and (2) train ten students (Members  
PDD 1/50197

USSR/Radio - Radio, Training (Contd) Sep 49

of Young Communist League) of the Third Women's  
School in the principles of radio engineering,  
and assist them in constructing a school PA  
receiving unit.

PDD 1/50197

RYAZANTSEV, Yu.

Communist youth organization in an automobile and motorcycle club.  
Za rul. 20 no.3:2 Mr '62. (MIRA 15:3)

1. Neshtatnyy zamestitel' nachal'nika avtomotokluba g. Volnovakha,  
Donetskaya oblast'.  
(Volnovakha--Communist Youth League)

27264

S/020/61/139/005/018/021  
B103/B208

11.7200

AUTHORS: Novikov, S. S., and Ryazantsev, Yu. S.

TITLE: Interaction of the weak entropy wave with the flame front

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 139, no. 5, 1961, 1157-1158

TEXT: Contrary to the hypothesis that the propagation velocity of the flame remains unchanged on interaction of a flame front with the contact burst (G. M. Bam-Zelikovich, Teoreticheskaya gidromekhanika, sborn. (Theoretical hydromechanics, Collection), No. 4 (1949); Boa Te-Chu. Sborn. Voprosy gorenija i detonatsionnykh voln (Collection, Problems of burning and of detonation waves) M., 1958, str. 411), it was confirmed experimentally (S. M. Kogarko, ZhTF, 30, 1110 (1960)) that on interaction of a flame front with compression waves the latter may be intensified. This is explained by a change of the flame velocity during interaction (S. M. Kogarko, V. I. Skobelkin, DAN, 120, No. 6, 1280 (1958)). The interaction of a flame front with the entropy wave was studied considering the change of the propagation velocity of the flame due to the entropy wave. The authors assumed the entropy wave to be weak, and used the linear approxima-

Card 1/5

27264

S/020/61/139/005/018/021  
B103/B208

Interaction of the weak...

tion. The system formed by interaction of waves is shown in Fig. 1. The perturbation in a combustible mixture consists of an arriving entropy wave  $\delta q_1^e$  and the resultant pressure wave  $\delta p_1$ . The following waves will be formed in the products of combustion: The entropy wave  $\delta q_2^e$  and the pressure wave  $\delta p_2$ . These perturbations are interrelated by the equations of conservation of mass, momentum, and energy at the flame front. If the low values of an order of  $(U/c_1)^2$  and more ( $U$  being the propagation velocity of the flame, and  $c_1$  the sonic velocity), are neglected in these equations, one obtains:  $q_1 \delta U + U \delta q_1 + U \delta q_1^e = q_2 (\delta u_1 - \delta u_2 + \delta U) + q_1/q_2 U \delta q_2 + q_1/q_2 U \delta q_2^e$ ;  $\delta p_1 = \delta p_2 + 2q_1 U (\delta u_1 - \delta u_2)$ ;  $\delta w_1 + \delta w_1^e + U \delta U = \delta w_2 - \delta w_2^e + q_1/q_2 U (\delta u_1 - \delta u_2 + \delta U)$ . (1). Besides, the following interrelations hold for waves: The falling entropy wave:  $\delta w_1^e = -[c_1^2/q_1 (\gamma_1 - 1)] \delta q_1^e$ ; the pressure wave in the combustible mixture:  $\delta u_1 = c_1/\gamma_1 \delta p_1/p_1 = \delta q_1 - \delta p_1/c_1^2$ ;

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S/020/61/139/005/018/021  
B103/B208

Interaction of the weak...

the pressure wave in the products of combustion:  $\delta u_2 = -(c_2/\gamma_2)(\delta p_2/p_2)$ ,  
 $\delta q_2 = \delta p_2/c_2^2$ ; the entropy wave in the products of combustion:  $\delta w_2^e$   
 $= - [c_2^2/\rho_2(\gamma_2 - 1)] \delta q_2^e$  (2). The authors state that the change of the  
 propagation velocity of the flame is related to the change of the thermo-  
 dynamic parameters of the combustible mixture as follows:  $\delta U = A\delta p_1 + B\delta q_1^e$   
 (3), where  $A = (\partial U/\partial p_1)_{T_1} + [(\gamma_1 - 1)/\gamma_1] (T_1/p_1) (\partial U/\partial T_1)_{p_1}$ ;  
 $B = -c_1^2 [\rho_1 c_{p_1} (\gamma_1 - 1)] (\partial U/\partial T_1)_{p_1}$ . The function  $U(p_1, T_1)$  is considered  
 to be determined experimentally or theoretically. Using (1), (2) and (3),  
 the authors obtain: for the pressure wave in the combustible mixture

$$\delta p_1 = \frac{[(p_1 - p_2) c_2 B + U c_2 - \frac{\gamma_2 - 1}{\gamma_1 - 1} c_1^2 \frac{U}{c_2}] \delta p_1^e}{\left\{ 1 + \frac{p_2 c_2}{p_1 c_1} - (p_1 - p_2) c_2 A - \left[ (\gamma_2 - 1) \frac{c_1}{c_2} + 2 - (\gamma_2 - 3) \frac{c_2}{c_1} \right] \frac{U}{c_1} \right\}}; \quad (4)$$

for the pressure wave in the products of combustion

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S/O20/61/139/005/018/021  
B103/B208

Interaction of the weak...

$$\delta p_2 = \frac{\left[ (\rho_1 - \rho_2) c_2 B + U c_2 - \frac{\gamma_2 - 1}{\gamma_1 - 1} c_1^2 \frac{U}{c_2} - 2(\rho_1 - \rho_2) c_2 B \left( 1 + \frac{c_2}{c_1} \right) \frac{U}{c_1} \right] \delta p_1^2}{\left\{ 1 + \frac{\rho_2 c_2}{\rho_1 c_1} - (\rho_1 - \rho_2) c_2 A - \left[ (\gamma_2 - 1) \frac{c_1}{c_2} + 2 - (\gamma_2 - 3) \frac{c_2}{c_1} \right] \frac{U}{c_1} \right\}}, \quad (5),$$

and for the entropy wave in the products of combustion  $\delta p_2^e \equiv \delta p_2^e$ . If a perturbation of the heat supply  $\delta Q$  occurs in the combustible mixture, the values for  $\delta p_1$ ,  $\delta p_2$ , and  $\delta Q_2^e$  may be determined.  $\delta U = A \delta p_1 + D \delta Q$ , where  $D = (\partial U / \partial Q)_{p_1, T_1}$ . Hence, (7) is expressed as follows:

$$\delta p_1 = \frac{\left[ (\rho_1 - \rho_2) c_2 D + (\gamma_2 - 1) \rho_2 \frac{U}{c_2} \right] \delta Q}{\left\{ 1 + \frac{\rho_2 c_2}{\rho_1 c_1} - (\rho_1 - \rho_2) c_2 A - \left[ (\gamma_2 - 1) \frac{c_1}{c_2} + 2 - (\gamma_2 - 3) \frac{c_2}{c_1} \right] \frac{U}{c_1} \right\}}. \quad (7)$$

The occurrence of perturbations  $\delta Q_1^e$  and  $\delta Q$  in the combustible mixture results in waves whose intensity equals the sum of wave intensities which are caused by each of these perturbations. The expressions of the intensity of pressure waves which are given in Ref. 2, may be derived from (4)  
Card 4/5

27264

Interaction of the weak...

S/020/61/139/005/018/021  
B103/B208

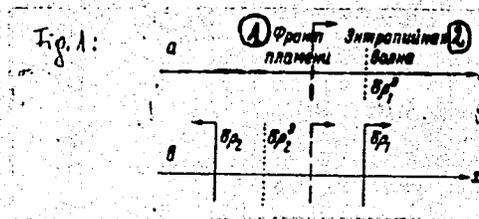
and (7) if the variation of the propagation velocity of the flame is zero. There are 1 figure and 5 Soviet-bloc references.

ASSOCIATION: Institut khimicheskoy fiziki Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences USSR).

PRESENTED: March 11, 1961 by V. N. Kondrat'yev, Academician

SUBMITTED: March 8, 1961

Legend to Fig. 1: (1) Flame front, (2) entropy wave.



Card 5/5

35754

S/207/62/000/002/013/015  
D237/D302

11.72-00

AUTHOR: Ryazantsev, Yu. S. (Moscow)

TITLE: Reflection of the shock-wave from a burning surface

PERIODICAL: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki,  
no. 2, 1962, 122-123

TEXT: Assuming that the infinitely thin zone of the chemical reaction coincides with the surface of the condensed phase and that the mass rate of burning depends on the pressure only and is

$$\rho_0 U = A p^{\nu} \quad (1)$$

where  $\rho_0$  - density of condensed phase,  $U$  - linear burning velocity,  $p$  - pressure,  $A$  and  $\nu$  - constants, the author gives the relations for the pressures, densities and velocities on the incident and reflected wave, on the combustion front before and after the

Card 1/2

Reflection of the ...

S/207/62/000/002/013/015  
D237/D302

contact and on the shock discontinuity and establishes that for  $v \leq 1$ ; the intensity of the reflected shock-wave is less than that obtained on reflection from a perfectly rigid body. The author also obtains an expression for the coefficient of reflection of a weak pressure wave from a burning surface and in conclusion notes that under non-stationary conditions, the law of combustion of the type (1) may not be fulfilled. There are 2 figures and 2 Soviet-bloc references.

SUBMITTED: January 13, 1962

Card 2/2

30040  
S/040/62/026/002/022/025  
D299/D301

24.4300

AUTHORS: Novikov, S.S., and Ryazantsev, Yu.S. (Moscow)

TITLE: On the reflection of plane sound waves from the open end of a circular tube

PERIODICAL: Prikladnaya matematika i mekhanika, v. 26, no. 2, 1962  
376 - 380

TEXT: A formula is derived for the reflection coefficient of a plane sound-wave from the open end of a circular, semi-infinite tube with absolutely rigid walls; the contact discontinuity at the boundary combustion flow - surrounding medium, is taken into account. The reflection coefficient is required in the study of vibrational combustion. The axis of the unflanged tube, of radius a, coincides with the z-axis of a cylindrical system of coordinates (r, z); axial symmetry is assumed. Steady oscillations are considered; the time-dependence of the acoustic field is described by a function of type  $\exp(-i\omega t)$ . The equations of the acoustic field are:

$$\Delta \Psi_j + k_j^2 \Psi_j = 0 \quad (j = 1, 2; k_j^2 = \frac{\omega^2}{c_j^2}; \Delta = \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial}{\partial r}) + \frac{\partial^2}{\partial z^2}) \quad (1) \checkmark$$

Card 1/4

S/040/62/026/002/022/025  
D299/D301

On the reflection of plane sound ...

where  $c_j$  is the velocity of sound, and  $\Psi_j$  is the velocity potential. The boundary conditions are set up. The sought-for coefficient of reflection is expressed as the ratio  $R = B/A$  (of the amplitude  $B$  of the reflected wave, to the amplitude  $A$  of the incident wave). After transformations, one obtains

$$z_1^2 L(\zeta) H(\zeta) = \frac{2}{a} W(\zeta) \tag{15}$$

$$L(\zeta) = \frac{2\rho_{01} J_1(a z_1) H_1^{(1)}(a z_2) z_2 / z_1}{\rho_{01} a z_2 J_0(a z_1) H_1^{(1)}(a z_2) - \rho_{02} a z_1 J_1(a z_1) H_0^{(1)}(a z_2)} \quad (z_j = \sqrt{k_j^2 - \zeta^2}) \tag{16}$$

where  $H$  is Hankel's function and  $J$  - Bessel's function. For convenience, it is assumed that the constants  $k_j$  are complex numbers. It is shown that

$$R = \frac{\text{res}_{\zeta = -k_1} H(\zeta)}{\text{res}_{\zeta = k_1} H(\zeta)} \tag{17}$$

From the asymptotic values of the function  $\Psi_1$ , for  $z \rightarrow \infty$ , follows that  
Card 2/4

On the reflection of plane sound ...

S/040/62/026/002/022/025  
D299/D301

$$H(\zeta) = -\frac{iA}{\zeta - k_1} - \frac{iB}{\zeta + k_1} + \varphi(\zeta). \quad (18)$$

Hence (17) holds. Thus, the problem reduces to determining the function  $H(\zeta)$  from Eq. (15). This equation is solved by the Wiener-Hopf method. One obtains

$$H(\zeta) = \frac{\text{const}}{(k_1^2 - \zeta^2)L_+(\zeta)}. \quad (27)$$

From

$$R = /R/e^{2i\delta} = - [L_+(k_1)]^2 \quad (29)$$

one obtains the formula for the reflection coefficient. If the frequency  $\omega$  and the radius  $a$  are small (so that  $k_j a \ll 1$ ), then the obtained formula is simplified, by retaining only the first terms in the expansion of cylindrical functions; thereupon integration yields:

$$/R/ = \exp\left[-\frac{k_1 k_2 a^2}{2} \frac{\rho_{02}}{\rho_{01}}\right] \quad (32) \quad \checkmark$$

Card 3/4

On the reflection of plane sound ...

S/040/62/026/002/022/025  
D299/D301

This formula holds for  $k_2 > k_1$ . If the medium is homogeneous, Eq. (32) simplifies still further. It is noted that, according to Eq. (32) in case of a hot flow and a cold medium, the radiation from the open end is larger (i.e.  $R$  is smaller) than that in a homogeneous medium, regardless of whether the medium is characterized by the parameters 1 or 2. There are 2 figures and 12 references: 6 Soviet-bloc and 6 non-Soviet-bloc (including 4 translations); The references to the English-language publications read as follows: H. Levine, I. Schwinger, On the radiation of sound from unflanged circular pipe. Phys. Rev., 1948, v. 73, no. 4; G.F. Carrier, Sound transmission from tube with flow. Quart. Appl. Math., 1956, v. 13.

SUBMITTED: December 25, 1961

Card 4/4

RYAZANTSEV, Yu.S. (Moskva)

Allowing for density changes in phase transformation in Stefan's  
problem. Prikl. mat. i mekh. 25 no.6:1143-1144 N-D '61.

(MIRA 14:12)

(Phase rule and equilibrium) (Thermodynamics)

NOVIKO, S.S.; RYAZANTSEV, Yu.S.

Interaction between a weak entropy wave and the flame front.  
Dokl. AN SSSR 139 no.5:1157-1158 Ag. '61. (MIRA 14:8)

1. Institut khimicheskoy fiziki AN SSSR. Predstavleno  
akademikom V.N. Kondrat'yevym.  
(Combustion research) (Entropy)

S/207/61/000/006/009/025  
A001/A101

11.7300

AUTHORS: Novikov, S.S., Ryazantsev, Yu.S. (Moscow)

TITLE: Acoustic conductivity of a stable burning surface

PERIODICAL: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 6, 1961,  
73 - 77

TEXT: The authors consider the plane front of burning, which coincides with the surface of the condensed phase (assumed to be incompressible), under conditions of mass, momentum and energy conservation. They derive an expression for acoustic conductivity, being the ratio of the normal component of acoustic velocity to acoustic pressure, taking into consideration perturbations in the combustion products (which are assumed to be a perfect gas) composed of incident and reflected waves of pressure and entropy wave. Conclusions are drawn as follows: 1) if the stationary law of burning is fulfilled under unstationary conditions, the stable burning surface is acoustically stable; 2) the region of acoustic stability changes essentially when entropy waves, arising in an interaction of acoustic waves with the burning surface, are taken into account; 3) amplification of a weak pressure wave in interaction with a stable burning surface is possible

Card 1/2

Acoustic conductivity of a stable burning surface

S/207/61/000/006/009/025  
A001/A101

only if the non-stationary combustion law satisfies certain requirements. The authors are of the opinion that existent attempts to establish this law have been unsatisfactory and formulate demands on such a law. The following Soviet-bloc personalities are mentioned: Ya.B. Zel'dovich and A.F. Belyayev. The authors thank A.D. Margolin for a discussion of the present work. There are 17 references, 13 of which are Soviet-bloc. ✓B

SUBMITTED: April 15, 1961

Card 2/2

28675

S/020/61/140/002/020/023  
B101/B110

11.7300

AUTHORS: Novikov, S. S., and Ryazantsev, Yu. S.

TITLE: Model of unstable combustion

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 140, no. 2, 1961, 409-411

TEXT: The authors looked for a possibility of avoiding the experimental difficulties in measuring the acoustic impedance of a burning surface. They proceeded from a linear (tubular) model in which instabilities may appear in the longitudinal direction only. In linear approximation, the problem of instability of combustion of a condensed system in a tube is regarded as an acoustic problem of natural oscillations in the tube between the impedances  $Z_0$  and  $Z_1$ . Assuming a low combustion rate, the change of the free tube length is neglected. The following relation holds for the eigenfrequencies:  $(Z_0 + 1)/(Z_0 - 1) = (Z_1 - 1)/(Z_1 + 1) \exp(-2ikl)$  (1).  $k = \omega/c$  is the wave vector,  $Z_0$  the impedance of the burning surface,  $Z_1$  the impedance of the open tube end. The following

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S/020/61/140/002/020/023  
B101/E110

Model of unstable combustion

condition is written for the self-excitation of the system:  $r_0 r_1 > 1$  (2), where  $r_0 = |R_0|$ ;  $R_0 = r_0 \exp(2i\delta_0)$  is the reflection coefficient of the burning surface.  $r_1 = |R_1|$ ;  $R_1 = r_1 \exp(2i\delta_1)$  is the reflection coefficient of the open tube end. If  $Z_0$  and  $Z_1$  are known, it is possible to calculate the critical  $\omega_{cr}$ ,  $l_{cr}$  for the limit combustion stability. If the system has a range of instability, it is possible to calculate the impedance  $Z_0$  from  $\omega_{cr}$ ,  $l_{cr}$ . Reference is made to L. Ya. Gutin, ZhTF, 7, 10, 1097 (1937), for the calculation of  $Z_1$ . The determination of  $\omega_{cr}$ ,  $l_{cr}$  for various tube diameters yields the frequency dependence  $Z_0(\omega)$ . If  $Z_0$  is independent of  $\omega$ , and  $r_0 > 1$ , then: (a) combustion is stable with  $l < l_{cr}$ ; (b) with increasing combustion of the condensed phase, the eigenfrequency drops and finally reaches:  $\omega_{cr} = (c/a) \sqrt{1 - 1/r_0^2}$ . At that instant combustion becomes unstable, and the system produces sound vibrations. There are 1 figure and 13 references: 9 Soviet and 4 non-Card 2/3

Model of unstable combustion

28675  
S/020/61/140/002/020/023  
B101/B110

Soviet. The four references to English-language publications read as follows: H. Grad, Comm. on Pure and Appl. Math., 2, 79 (1949); F. T. McClure, R. W. Hart, J. F. Bird, J. Appl. Phys., 31, 884 (1960); J. F. Bird, L. Haar, R. W. Hart, F. T. McClure, J. Chem. Phys., 32, 1423 (1960); W. Maxwell, Fourth Symposium on Combustion, 1953. X

ASSOCIATION: Institut khimicheskoy fiziki Akademii nauk SSSR (Institute of Chemical Physics of the Academy of Sciences USSR)

PRESENTED: April 13, 1961, by V. N. Kondrat'yev, Academician

SUBMITTED: April 10, 1961

Card 3/3

NOVIKOV, S.S.; RYAZANTSEV, Yu.S.

Model of unsteady burning. Dokl. AN SSSR 140 no.2:409-411 S '61.  
(HIRA 14:9)

1. Institut khimicheskoy fiziki AN SSSR. Predstavleno akademikom  
V.N.Kondrat'yevym.

(Combustion)

23856

S/020/61/137/006/018/020  
B101/B201

11.7200

AUTHORS: Novikov, S. S. and Ryazantsev, Yu. S.

TITLE: Interaction of weak pressure waves with the flame front

PERIODICAL: Doklady Akademii nauk SSSR, v. 137, no. 6, 1961, 1409-1412

TEXT: This is a gas-dynamic study of the non-relaxing interaction of weak pressure waves with the flame front on a change of the thermodynamic parameters of the burning mixture in the weak wave. A) If the pressure wave catches up with the flame front, a pressure wave and an entropy wave are reflected after interaction with the flame, while the wave that has passed through the flame goes on propagating. For the conservation of mass, momentum, and energy at the front of flame the following relations are written:  $q_1 U = p_2(u_1 - u_2 + U)$ ;  $p_1 + q_1 U^2 = p_2 + q_2(u_1 - u_2 + U)^2$ ;  $w_1 + U^2/2 = w_2 + (u_1 - u_2 + U)^2/2$  (1). By retaining the terms of zeroth and minus first order with respect to  $U/c_1$  ( $U =$  propagation rate of flame,  $c_1 =$  sound velocity) the following is written:

X

Card 1/6

23856

S/020/61/137/006/018/020  
B101/B201

Interaction of weak ...

$$\begin{aligned}
 & q_1 \delta U + U \delta q_1^{\text{pass}} = q_2 (\delta u_1^{\text{pass}} - \delta u_2^{\text{inc}} - \delta u_2^{\text{refl}} + \delta U) + (U c_2^2 / c_1^2) (\delta q_2^{\text{inc}} + \delta q_2^{\text{refl}} \\
 & + \delta q_2^{\text{entr}}); \delta p_1^{\text{pass}} + 2 q_1 U \delta U = \delta p_2^{\text{inc}} + \delta p_2^{\text{refl}} + 2 q_2 U (c_2^2 / c_1^2) (\delta u_1^{\text{pass}} - \delta u_2^{\text{inc}} \\
 & - \delta u_2^{\text{refl}} + \delta U); \delta w_1^{\text{pass}} + U \delta U = \delta w_2^{\text{inc}} + \delta w_2^{\text{refl}} + \delta w_2^{\text{entr}} + U (c_2^2 / c_1^2) (\delta u_1^{\text{pass}} \\
 & - \delta u_2^{\text{inc}} - \delta u_2^{\text{refl}} + \delta U) \quad (2).
 \end{aligned}$$

Here, inc means incident pressure wave; pass: passed pressure wave, refl: reflected pressure wave, entr: entropy wave. The following relations holds: incident pressure wave

$$\delta S_2^{\text{inc}} = 0; \delta u_2^{\text{inc}} = \delta p_2^{\text{inc}} / q_2 c_2; \delta w_2^{\text{inc}} = \delta p_2^{\text{inc}} / q_2; \delta q_2^{\text{inc}} = \delta p_2^{\text{inc}} / c_2^2 \quad (3);$$

$$\text{reflected pressure wave: } \delta S_2^{\text{refl}} = 0; \delta u_2^{\text{refl}} = -\delta p_2^{\text{refl}} / q_2 c_2;$$

$$\delta w_2^{\text{refl}} = \delta p_2^{\text{refl}} / q_2; \delta q_2^{\text{refl}} = \delta p_2^{\text{refl}} / c_2^2; \text{passed pressure wave:}$$

$$\delta S_1^{\text{pass}} = 0; \delta u_1^{\text{pass}} = \delta p_1^{\text{pass}} / q_1 c_1; \delta w_1^{\text{pass}} = \delta p_1^{\text{pass}} / q_1; \delta q_1^{\text{pass}} = \delta p_1^{\text{pass}} / c_1^2 \quad (5);$$

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for the entropy wave:  $\delta p_2^{entr} = 0; \delta u_2^{entr} = 0;$

$\delta w_2^{entr} = T_2 \delta S_2^{entr} = -c_2^2 \delta q_2^{entr} / q_2 (\gamma - 1)$  (6). The change  $\delta U$  of the

propagation velocity of the flame is, under the assumption that  $U = f(p_1, T_1)$

be known, found from:  $\delta U = (\partial f / \partial p_1)_{T_1} \delta p_1 + (\partial f / \partial T_1)_{p_1} \delta T_1 = A \delta p_1;$

$A = (\partial f / \partial p_1)_{T_1} + [(\gamma - 1) / \gamma] (T_1 / p_1) (\partial f / \partial T_1)_{p_1}$  (7). Introducing Eqs. (3)-

(7) into (2) and eliminating  $\delta q_2^{entr}$  gives:

$[(q_1 - q_2)A + U/c_1^2 + (\gamma - 1)U/c_2^2 - q_2/q_1 c_1] \delta p_1^{pass} = (\gamma U/c_1^2)(\delta p_2^{inc} + \delta p_2^{refl})$   
 $- (\delta p_2^{inc} - \delta p_2^{refl})/c_2; \delta p_1^{inc} = (1 + 2U/c_1)(\delta p_2^{inc} + \delta p_2^{refl}) - (2Uc_2/c_1^2)(\delta p_2^{inc}$

$- \delta p_2^{refl})$  (8). Thence, for the acoustic conductivity of the flame front,

is found:  $\zeta = q_2 c_2 / q_1 c_1 - (q_1 - q_2) c_2 A + (\gamma - 1)(1 - c_1^2 / c_2^2) U c_2 / c_1^2 + 2(q_1$

$- q_2) A [c_1 - (q_1 - q_2) A c_2^2] U c_2 / c_1^2$  (9). Between the reflection factor

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$k = \delta p_2^{refl} / \delta p_2^{inc}$  and  $\zeta$  holds the relation:  $k = (1 - \zeta) / (1 + \zeta)$ . The refractive index  $l$  results from Eq. (2):

$$l = \left[ \frac{2(1 + \zeta_0)}{1 + 2(\rho_1 - \rho_2)AUc_2^2/c_1^2 - BU/(1 + \zeta_0)c_1} \right] \quad (10), \text{ where}$$

$$\zeta_0 = \rho_2 c_2 / \rho_1 c_1 - (\rho_1 - \rho_2)c_2 A; B = \left\{ (\gamma - 1)(1 - c_1^2/c_2^2) + 2(\rho_1 + \rho_2)A \left[ c_1 - (\rho_1 - \rho_2)Ac_2^2 \right] \right\} c_2^2/c_1^2.$$

It follows from equation (9) that the acoustic conductivity of the flame constitutes in first approximation a sum, the individual terms of which correspond to different physical factors. B) If the incident wave moves toward the flame front, the following relations hold:

$$\zeta' = \rho_1 c_1 / \rho_2 c_2 - (\rho_1 - \rho_2)c_2 A c_2 / c_1 + (\gamma - 1)(1 - c_1^2/c_2^2)(Uc_2/c_2^2)(c_2/c_1) - 2(\rho_1 - \rho_2)AU(c_2/c_1)^3 \quad (11); l' = \left[ \frac{1}{1 + \zeta_0'} \right] \left[ 1 - 2(\rho_1 - \rho_2)AUc_2^2/c_1^2 \right]$$

-  $B'U/(1 + \zeta_0')c_1$  (12). Here as well, a discussion of the equations leads

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to the following conclusions: 1) in zeroth approximation ( $A = 0$ ) the flame has an acoustic conductivity being equal to the acoustic conductivity of the density discontinuity; 2) the physicochemical constant  $A$  takes account of the flame reaction to small perturbations. For  $q_1 \gg q_2$ , corresponding to the surface of burning condensed fuels, the acoustic conductivity of the flame is always negative:  $\zeta_c = -(q_1 - q_2)c_2A$  (13). The reflected wave is thus amplified. Eqs. (9)-(13) hold only for small values of  $A$ . With large  $A$  and under the action of weak waves, waves of finite intensity may arise in the flame, and the task is no more linear.  $A$  is the coefficient of the velocity of flame propagation with adiabatic pressure change in the combustible mixture.  $A$  may be calculated by the equation by Zel'dovich and Frank-Kamenetskiy (ZhFKh, 12, 1, 100 (1938)). For a methane-air mixture (10%  $CH_4$ ),  $T_0 = 20^\circ C$ ,  $P = 1$  atm;  $T_{burn} = 2100^\circ C$ ,  $\Delta U/\Delta T = 0.2$  cm/sec.deg the change in the velocity of flame propagation would amount to about 0.5%. In some cases, this change may, however, rise to some percent; this may have a considerable effect if the pressure wave, in consequence of reflections, passes through the flame front several times. There are 1 figure and

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ASSOCIATION: Institut khimicheskoy fiziki Akademii nauk SSSR (Institute of  
Chemical Physics, Academy of Sciences, USSR)

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SUBMITTED: December 3, 1960

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УДК 544.1

27 21  
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 the disagreement on the compn. and instability const. of  
 the Cd thiosulfate complexes found by potentiometric and  
 polarographic methods, the compn. and stability of the  
 $Cd^{++}S_2O_3^{--}$  complex were studied by the soly. method.

The soly. of  $Cd(OH)_2$  in water at  $25 \pm 0.1^\circ$  was  $1.75 \times 10^{-4}$  mol./l. The soly. of  $Cd(OH)_2$  in  $0.0297-0.0303M$  solns. of  $Na_2S_2O_3$  at the same temp. was measured. Increase in soly. of  $Cd(OH)_2$  with increase in concn. of  $Na_2S_2O_3$  was accepted as a proof of complex formation in the system. The instability const. and the no. of coordinated groups were calcd. by 2 methods. The no. of coordinated

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Investigated the composition and stability of the  $[TlS_2O_3]^-$  complex ion. Determined the solubility of  $Tl_2S_2O_3$  in Na S O solutions of various concentrations at  $25^\circ$ . From this data, the number of coordination groups in the formed complex ion were calculated. Na  $[TlS_2O_3]$  was synthesized from a concentrated solution of  $Na_2S_2O_3$  and a saturated solution of  $Tl_2S_2O_3$ . The product was in gel form and was readily soluble in water. K  $[TlS_2O_3]$  was prepared in crystalline form.

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